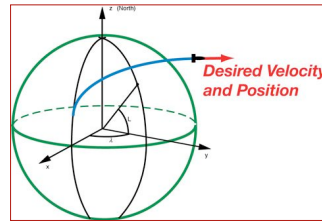


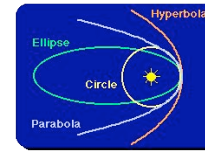
Launch Vehicle Design: Trajectories and Aerodynamics

Space System Design, MAE 342, Princeton University
Robert Stengel

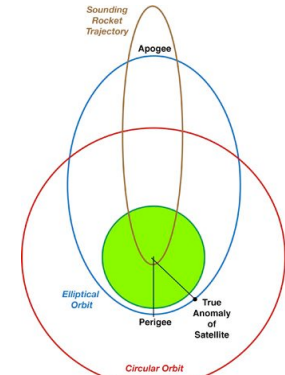
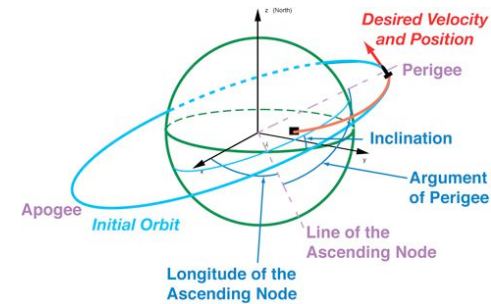
- Launch trajectories and effects
- Forces, moments, and stability
- Point mass, rigid body, and body bending



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<http://www.princeton.edu/~stengel/MAE342.html>



Final Position and Velocity Determine Orbital Elements



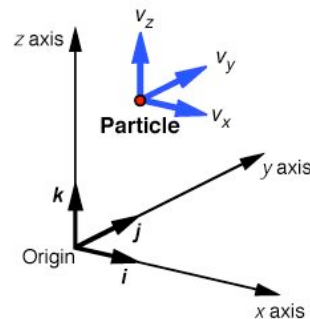
Position and Velocity

- Position of a particle

$$\mathbf{r} = \begin{bmatrix} x \\ y \\ z \end{bmatrix}$$

- Velocity of a particle

$$\mathbf{v} = \frac{d\mathbf{r}}{dt} = \dot{\mathbf{r}} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}$$



Newton's Laws of Motion: Dynamics of a Particle

- First Law
 - If **no force** acts on a particle, it **remains at rest** or continues to move in a straight line at **constant velocity**, as observed in an inertial reference frame -- **Momentum is conserved**
- Second Law
 - A particle of fixed mass **acted upon by a force** changes velocity with an **acceleration** proportional to and in the direction of the force, as observed in an inertial reference frame; the ratio of force to acceleration is the **mass** of the particle: **F = m a**
- Third Law
 - For every **action**, there is an equal and opposite **reaction**

$$\frac{d}{dt}(m\mathbf{v}) = 0 \quad ; \quad m\mathbf{v}|_{t_1} = m\mathbf{v}|_{t_2}$$

$$\frac{d}{dt}(m\mathbf{v}) = m \frac{d\mathbf{v}}{dt} = \mathbf{F} \quad ; \quad \mathbf{F} = \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

$$\therefore \frac{d\mathbf{v}}{dt} = \frac{1}{m} \mathbf{F} = \begin{bmatrix} 1/m & 0 & 0 \\ 0 & 1/m & 0 \\ 0 & 0 & 1/m \end{bmatrix} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

Equations of Motion for a Point Mass

$$\frac{d\mathbf{r}}{dt} = \dot{\mathbf{r}} = \mathbf{v} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}$$

$$\frac{d\mathbf{v}}{dt} = \dot{\mathbf{v}} = \frac{1}{m} \mathbf{F} = \begin{bmatrix} 1/m & 0 & 0 \\ 0 & 1/m & 0 \\ 0 & 0 & 1/m \end{bmatrix} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

Combined Equations of Motion for a Point Mass

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_y \\ \dot{v}_z \end{bmatrix} = \begin{bmatrix} v_x \\ v_y \\ v_z \\ f_x/m \\ f_y/m \\ f_z/m \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ y \\ z \\ v_x \\ v_y \\ v_z \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1/m & 0 & 0 \\ 0 & 1/m & 0 \\ 0 & 0 & 1/m \end{bmatrix} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

- With

$$\mathbf{F}_I = \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix} = \left[\mathbf{F}_{gravity} + \mathbf{F}_{aerodynamics} + \mathbf{F}_{thrust} \right]_I$$

Equations of Motion for a Point Mass

- Written as a single equation

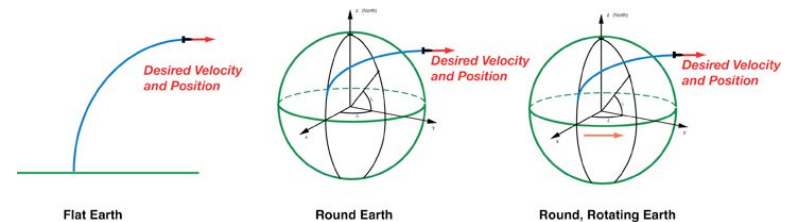
$$\dot{\mathbf{x}}(t) = \frac{d\mathbf{x}(t)}{dt} = \mathbf{f}[\mathbf{x}(t), \mathbf{F}]$$

- With

$$\mathbf{x} \equiv \begin{bmatrix} \mathbf{r} \\ \mathbf{v} \end{bmatrix} = \begin{bmatrix} x \\ y \\ z \\ v_x \\ v_y \\ v_z \end{bmatrix}$$

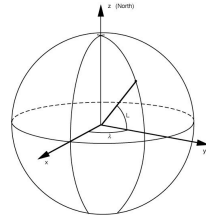
Newtonian Frame of Reference

- Newtonian (Inertial) Frame of Reference
 - Unaccelerated Cartesian frame whose origin is referenced to an inertial (non-moving) frame
 - Origin can translate at constant linear velocity
 - Frame cannot be rotating with respect to inertial origin
- ... but the Earth is rotating
 - Different approximations to “inertial” suit different problems





Force due to Gravity



- **Flat-earth approximation**
 - \mathbf{g} is gravitational **acceleration**
 - $m\mathbf{g}$ is gravitational **force**
 - **Independent of position**
- **Round, rotating earth**
 - Inverse-square gravitation
 - “Centrifugal acceleration”
 - **Non-linear function of position**
 - $\mu = 3.986 \times 10^{14} \text{ m}^3/\text{s}^2$
 - $\Omega = 7.29 \times 10^{-5} \text{ rad/s}$

$$m\mathbf{g}_f = m \begin{bmatrix} 0 \\ 0 \\ g_o \end{bmatrix}; \quad g_o = 9.807 \text{ m/s}^2$$

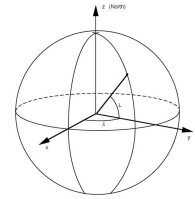
$$\mathbf{g}_r = \begin{bmatrix} g_x \\ g_y \\ g_z \end{bmatrix} = \mathbf{g}_{gravity} \quad [\text{non-rotating frame}]$$

$$\mathbf{g}_r = \mathbf{g}_{gravity} + \mathbf{g}_{rotation} \quad [\text{rotating frame}]$$

$$= \frac{-\mu}{r^3} \begin{bmatrix} x \\ y \\ z \end{bmatrix} - \Omega^2 \begin{bmatrix} x \\ y \\ 0 \end{bmatrix}; \quad r = [x^2 + y^2 + z^2]^{1/2}$$



Equations of Motion with Round-Earth Gravity Model (Inertial, Non-Rotating Frame)

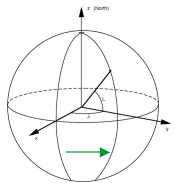


$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_y \\ \dot{v}_z \end{bmatrix}_E = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ -\mu/r^3 & 0 & 0 & 0 & 0 & 0 \\ 0 & -\mu/r^3 & 0 & 0 & 0 & 0 \\ 0 & 0 & -\mu/r^3 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ y \\ z \\ v_x \\ v_y \\ v_z \end{bmatrix}_I + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1/m & 0 & 0 \\ 0 & 1/m & 0 \\ 0 & 0 & 1/m \end{bmatrix} \left[\begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}_{aero} + \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}_{thrust} \right]$$

- **Position of the vehicle (in spherical coordinates)**

$$\mathbf{r} = \begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} \cos L \cos \lambda \\ \cos L \sin \lambda \\ \sin L \end{bmatrix} (R + h)$$

R : Earth's radius
 h : Altitude (height)
 L : Latitude
 λ : Longitude

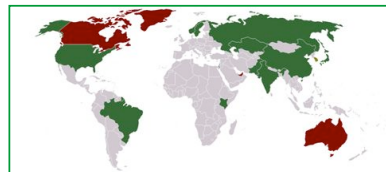
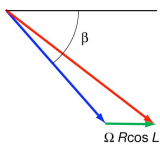


Effect of Launch Site on Launch Velocity

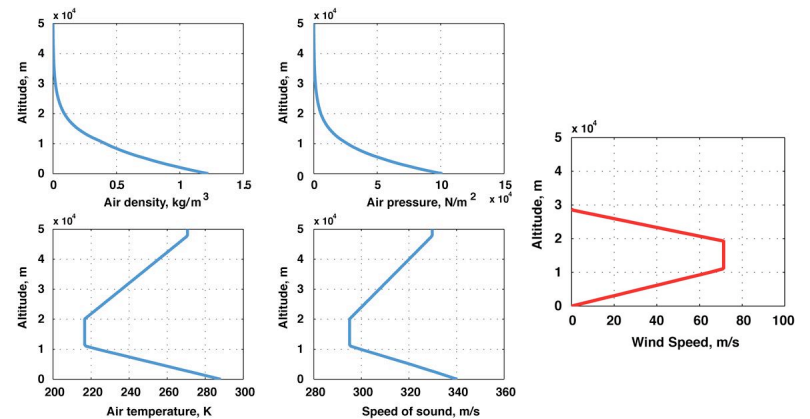
- **Launch site and azimuth**
 - Earth's rotation adds up to 465 m/s to final inertial velocity
 - **Function of launch latitude and azimuth angles**

$$\Delta V_{launch} \approx \Omega R \cos L \cos \beta$$

β : Launch azimuth angle (from East)



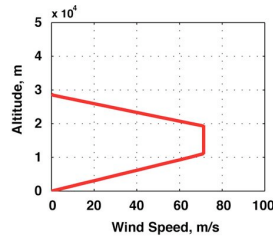
Properties of the Lower Atmosphere



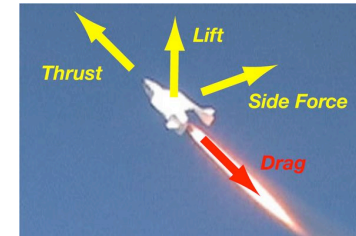
- **Air density and pressure decay exponentially with altitude**
- **Air temperature and speed of sound are linear functions of altitude**
- **Jet stream magnitude typically peaks at 10-15-km altitude**

Lower Atmosphere Rotates With The Earth

- Zero wind at Earth's surface = Inertially rotating air mass
- Wind measured with respect to Earth's rotating surface



Aerodynamic Forces



$$\begin{bmatrix} \text{Drag} \\ \text{Side Force} \\ \text{Lift} \end{bmatrix} = \begin{bmatrix} C_D \\ C_Y \\ C_L \end{bmatrix} \frac{1}{2} \rho V^2 S \approx \begin{bmatrix} \text{Axial Force} \\ \text{Side Force} \\ \text{Normal Force} \end{bmatrix} = \begin{bmatrix} C_A \\ C_Y \\ C_N \end{bmatrix} S \bar{q}$$

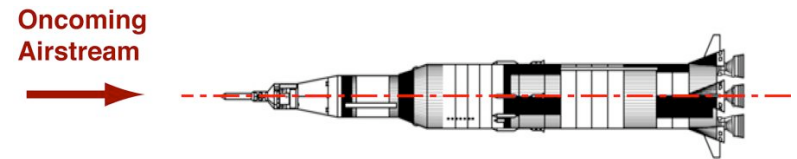
- V = air-relative velocity = velocity w.r.t. air mass
- Drag measured opposite to the air-relative velocity vector
- Lift and side force are perpendicular to the velocity vector

Aerodynamic Forces

$$\begin{aligned} \rho &= \text{air density, function of height} \\ &= \rho_{\text{sea level}} e^{-\beta z} \\ \rho_{\text{sea level}} &= 1.225 \text{ kg/m}^3; \quad \beta = 1/9,042 \text{ m} \\ V &= [v_x^2 + v_y^2 + v_z^2]^{1/2} = [\mathbf{v}^T \mathbf{v}]^{1/2} \\ \text{Dynamic pressure} &= \bar{q} = \frac{1}{2} \rho V^2 \\ S &= \text{reference area, m}^2 \\ \begin{bmatrix} C_D \\ C_Y \\ C_L \end{bmatrix} &= \text{non-dimensional aerodynamic coefficients} \end{aligned}$$

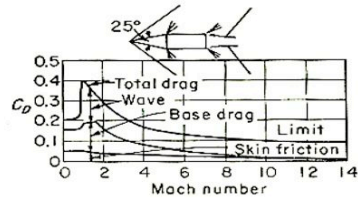
Aerodynamic Drag

$$\text{Drag} = C_D \frac{1}{2} \rho V^2 S$$

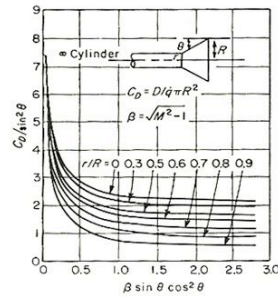


- Drag components sum to produce total drag
 - Skin friction
 - Base pressure differential
 - Forebody pressure differential ($M > 1$)

Drag Coefficients of Cones and Cone Frustums

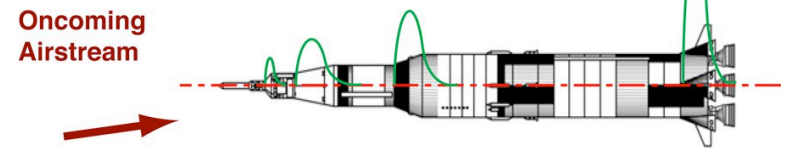


$$M = \frac{\text{Air - Relative Velocity}}{\text{Speed of Sound}}$$



Aerodynamic Lift Force

$$\text{Lift} = C_L \frac{1}{2} \rho V^2 S \approx \frac{\partial C_L}{\partial \alpha} \alpha \frac{1}{2} \rho V^2 S$$



- Angle between x axis and airstream = angle of attack, α
- Lift components integrate over length to produce net lift
 - Increase in cross-sectional area
 - Tail fins
- For symmetric vehicle, lift = 0 if $\alpha = 0$

2-D Equations of Motion for a Point Mass

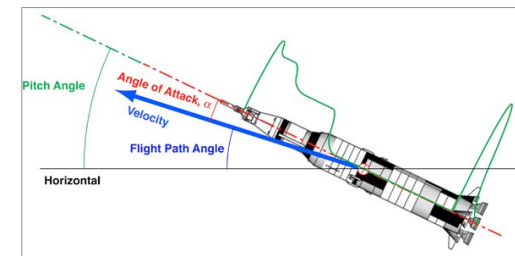
- Restrict motions to a vertical plane (i.e., motions in y direction = 0)

$$\begin{bmatrix} \dot{x} \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_z \end{bmatrix} = \begin{bmatrix} v_x \\ v_z \\ f_x/m \\ f_z/m \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ z \\ v_x \\ v_z \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1/m & 0 \\ 0 & 1/m \end{bmatrix} \begin{bmatrix} f_x \\ f_z \end{bmatrix}$$

2-D Equations of Motion for a Point Mass

- Transform velocity from Cartesian to polar coordinates

$$\begin{bmatrix} \dot{x} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} V \cos \gamma \\ -V \sin \gamma \end{bmatrix}; \quad \begin{bmatrix} V \\ \gamma \end{bmatrix} = \begin{bmatrix} \sqrt{\dot{x}^2 + \dot{z}^2} \\ -\sin^{-1}\left(\frac{\dot{z}}{V}\right) \end{bmatrix} = \begin{bmatrix} \text{Velocity} \\ \text{Flight path angle} \end{bmatrix}$$



Flat-Earth Model

- Ignore round, rotating Earth effects (!)
- i.e., assume that flat-Earth-relative frame is inertial

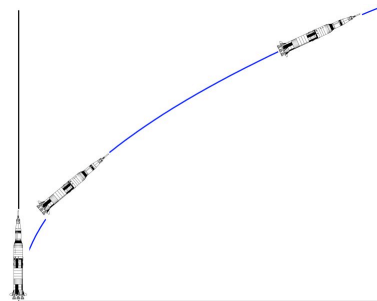
$$\begin{bmatrix} \dot{x} \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_z \end{bmatrix} = \begin{bmatrix} v_x \\ v_z \\ f_x/m \\ f_z/m \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ z \\ v_x \\ v_z \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1/m & 0 \\ 0 & 1/m \end{bmatrix} \begin{bmatrix} f_x \\ f_z \end{bmatrix}$$

$$\begin{bmatrix} \dot{x} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} V \cos \gamma \\ -V \sin \gamma \end{bmatrix}; \quad \begin{bmatrix} V \\ \gamma \end{bmatrix} = \begin{bmatrix} \sqrt{\dot{x}^2 + \dot{z}^2} \\ -\sin^{-1}\left(\frac{\dot{z}}{V}\right) \end{bmatrix} = \begin{bmatrix} \text{Velocity} \\ \text{Flight path angle} \end{bmatrix}$$

- Adequate model for investigating early phase of launch

Gravity-Turn Flight Path

- For vertical launch,
 - trajectory is vertical unless
 - vehicle is pitched over via thrust-vector control
- Following pitch-over,
 - if thrust is aligned with the velocity vector,
 - the result is called a **gravity turn**
- Gravity-turn flight path is a function of 3 variables
 - Initial pitch-over angle (from vertical launch)
 - Velocity at pitch-over
 - Acceleration profile, $T(t)/m(t)$



Simplified Launch Trajectory Equations of Motion

- **Gravity-turn, flat earth, vertical plane**
 - Thrust aligned with velocity vector ($\alpha = 0$)
 - Lift = 0
 - Round, rotating earth effects neglected

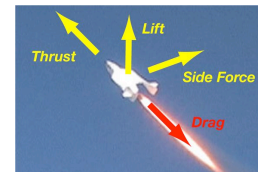
$$\dot{V}(t) = \frac{\text{Thrust} - [\text{Drag} + m(t)g \sin \gamma(t)]}{m(t)} = \left[\left(\text{Thrust} - C_D \frac{1}{2} \rho(h) V^2(t) \right) / m(t) - g \sin \gamma(t) \right]$$

$$\dot{\gamma}(t) = -g \cos \gamma(t) / V(t)$$

$$\dot{h}(t) = -\dot{z}(t) = V(t) \sin \gamma(t)$$

$$\dot{r}(t) = \dot{x}(t) = V(t) \cos \gamma(t)$$

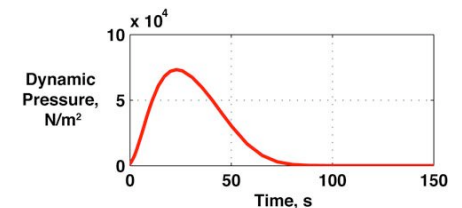
V = velocity
 γ = flight path angle
 h = height (altitude)
 r = range



Typical Velocity Loss due to Drag During Launch

- Aerodynamic effects on launch vehicle are most important below ~50-km altitude
- Maintain angle of attack and sideslip angle near zero to minimize side force and lift
- Typical velocity loss due to drag for **vertical launch**
 - Constant thrust-to-weight ratio
 - $C_D S/m = 0.0002 \text{ m}^2/\text{kg}$
 - Final altitude above 80 km

Thrust-to-Weight Ratio	Velocity Loss, m/s
2	336
3	474
4	581



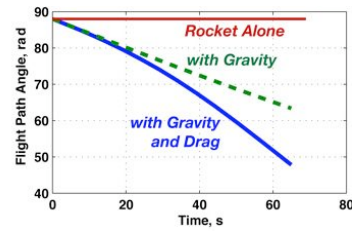
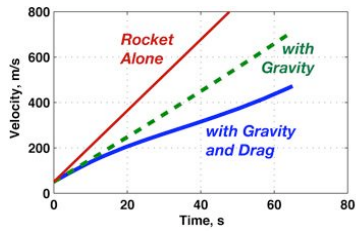


Effects of Gravity and Drag on the Velocity Vector

Thrust/Weight = $T/W = 2$
 Thrust = 1960
 $C_D = 0.2$
 $S = 0.1$
 Mass = 100

$$\dot{V}(t) = \frac{\text{Thrust} - \left[C_D S \frac{1}{2} \rho(h) V^2(t) + mg \sin \gamma(t) \right]}{m}$$

$$\dot{\gamma}(t) = -g \cos \gamma(t) / V(t)$$

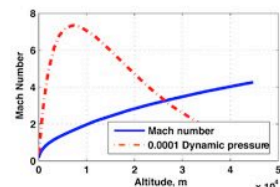
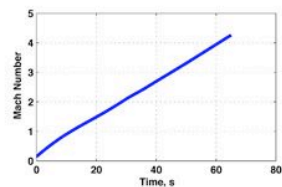
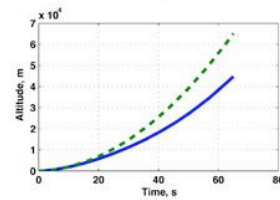
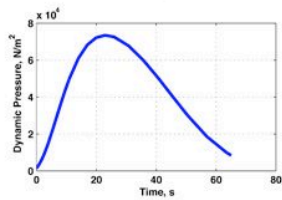
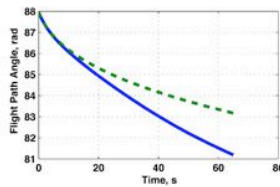
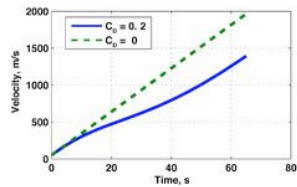
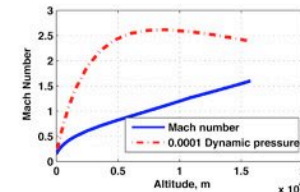
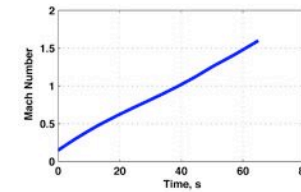
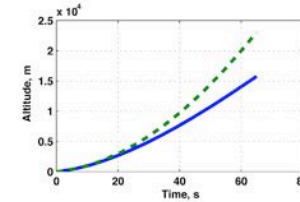
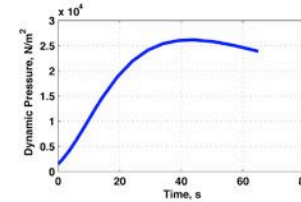
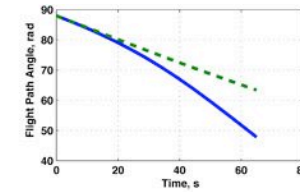
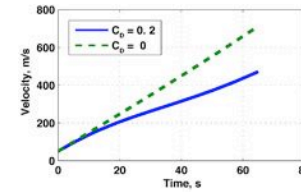


- Significant reduction in velocity magnitude
- Strong curvature of the flight path

Typical Properties of Launch Trajectories

Thrust/Weight = 2

- Maximum dynamic pressure, Mach = 1, maximum drag, and maximum jet stream magnitude tend to occur at similar altitudes
- Aerodynamic effects on launch vehicle become negligible above ~50-km altitude



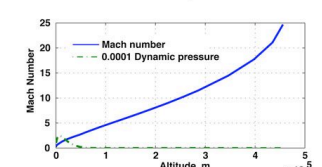
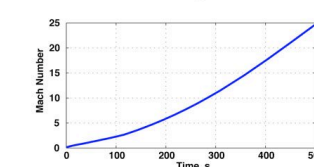
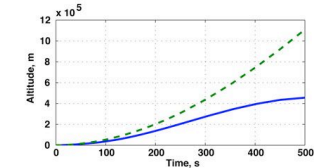
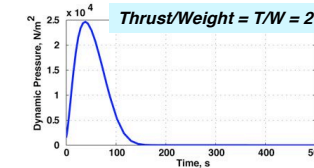
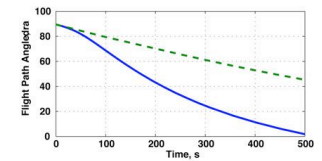
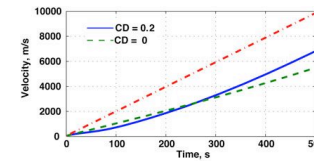
Typical Properties of Launch Trajectories

Thrust/Weight = 4

- Maximum dynamic pressure, Mach = 1, maximum drag, and maximum jet stream magnitude tend to occur at similar altitudes
- Aerodynamic effects on launch vehicle become negligible above ~50-km altitude

Gravity and Drag Effects during Single-Stage Orbital Launch

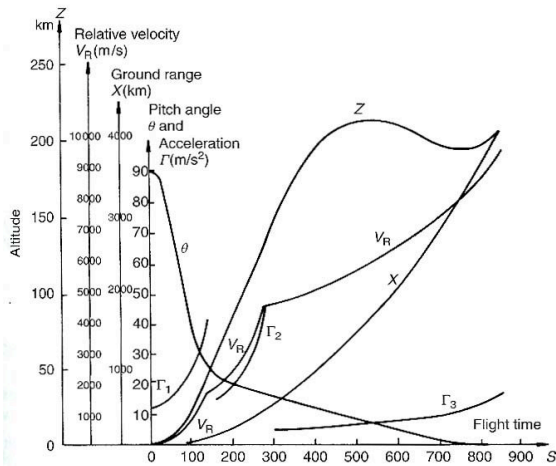
- Pseudo-orbital launch trajectory (using flat-earth model)
- Red line signifies velocity due to rocket alone
- Several km/s lost to gravity and drag



- With higher T/W
 - Shorter time to orbit
 - Increased loss due to drag
 - Decreased loss due to gravity

Typical Ariane 4 Launch Profile

(Spacecraft Systems Engineering, 2003)



Mass-Ratio Effect on Final Load Factor

- Thrust-to-weight ratio = load factor

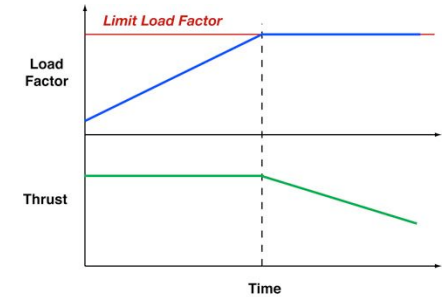
$$\frac{\text{Thrust}}{\text{Weight}} = n \text{ (load factor)} = \frac{\text{Thrust}}{mg_o}$$

$$n_{\text{initial}} = \frac{\text{Thrust}}{m_{\text{initial}}g_o}; \quad n_{\text{final}} = \frac{\text{Thrust}}{m_{\text{final}}g_o}$$

- If thrust is constant

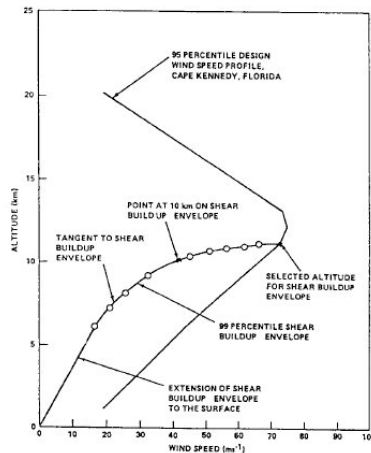
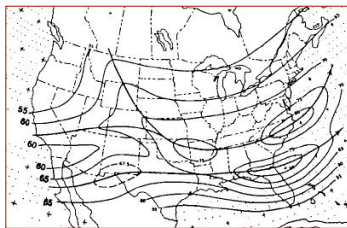
$$\frac{n_{\text{final}}}{n_{\text{initial}}} = \frac{m_{\text{initial}}}{m_{\text{final}}} = \mu$$

Initial Load Factor	Final Load Factor	Mass Ratio
1.3	2.6	2
2	4	2
3	6	2
	6.5	5
	10	5
	15	5



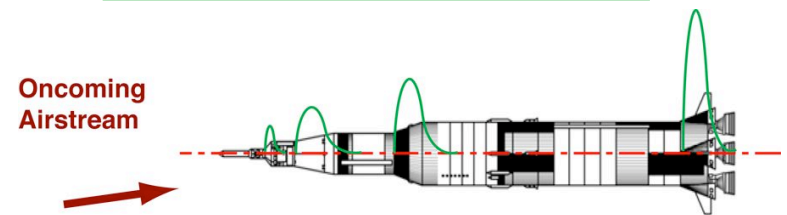
Jet Stream Profiles

- Launch vehicle must be able to fly through strong wind profiles
- Design profiles assume 95th-99th-percentile worst winds and wind shear



Aerodynamic Normal Force

$$\text{Normal Force} = C_N \frac{1}{2} \rho V^2 S \approx \frac{\partial C_N}{\partial \alpha} \alpha \frac{1}{2} \rho V^2 S$$

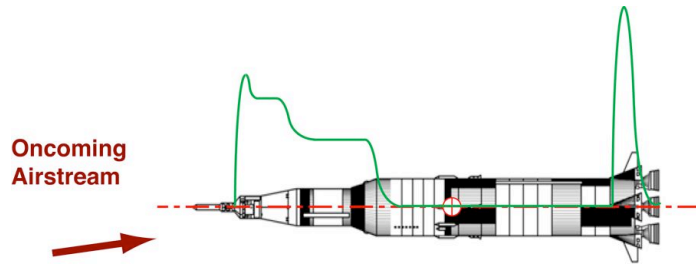


- For small angle of attack, normal force is approximately the same as lift

Aerodynamic Pitching Moment

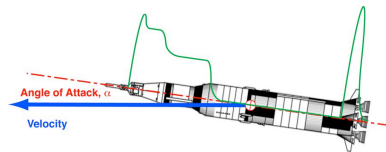
$$\text{Pitching Moment} = C_m \frac{1}{2} \rho V^2 S r \approx \frac{\partial C_m}{\partial \alpha} \alpha \frac{1}{2} \rho V^2 S r$$

$r = \text{Reference Length}$

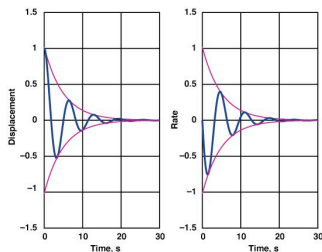


- Pitching moment components integrate over length to produce net pitching moment
 - Increase in cross-sectional area
 - Tail fins
- ... plus pitching moment due to thrust vectoring for control

Attitude Stability



$$\Delta \ddot{\alpha} = \frac{M_{y_{aero}} + M_{y_{thrust}}}{I_{yy}} \equiv \frac{M_{y_{net}}}{I_{yy}} \approx \frac{1}{I_{yy}} \left[\frac{\partial M_{y_{net}}}{\partial \dot{\alpha}} \Delta \dot{\alpha} + \frac{\partial M_{y_{net}}}{\partial \alpha} \Delta \alpha \right]$$



- Attitude perturbations are stable if

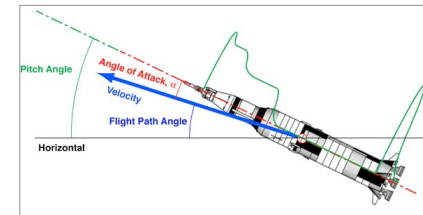
$$\frac{\partial M_{y_{net}}}{\partial \dot{\alpha}} < 0, \quad \frac{\partial M_{y_{net}}}{\partial \alpha} < 0$$
- Oscillatory divergence if

$$\frac{\partial M_{y_{net}}}{\partial \dot{\alpha}} > 0 \quad \text{Dynamic Instability}$$
- Non-oscillatory divergence if

$$\frac{\partial M_{y_{net}}}{\partial \alpha} > 0 \quad \text{Static Instability}$$

Thrust-vector feedback control normally required to provide static and dynamic stability

Angular Attitude Perturbations



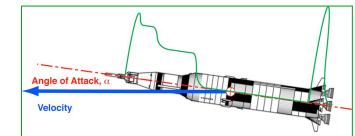
- Pitch-angle perturbation, $\Delta \theta$, is about the same as angle-of-attack perturbation, $\Delta \alpha$

$$\Delta \ddot{\theta} \approx \Delta \ddot{\alpha} = \frac{\text{Net Pitching Moment}}{\text{Pitching Moment of Inertia}}$$

- Then

$$\Delta \ddot{\alpha} = \frac{M_{y_{aero}} + M_{y_{thrust}}}{I_{yy}} \equiv \frac{M_{y_{net}}}{I_{yy}} \approx \frac{1}{I_{yy}} \left[\frac{\partial M_{y_{net}}}{\partial \dot{\alpha}} \Delta \dot{\alpha} + \frac{\partial M_{y_{net}}}{\partial \alpha} \Delta \alpha \right]$$

Typical Thrust-Vector Angle Requirements

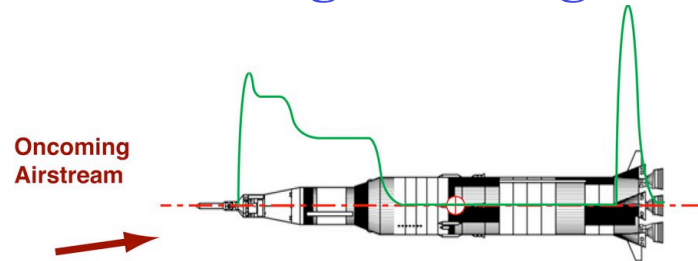


- Example: Concept study for solid-fueled Saturn-class vehicles (NASA TN D-4662, 1968)

Parameter	Variation	Deflection angle, deg		
		Apollo	Voyager	SSOPM
1. Steady stage winds	99 percent	1.35	2.30	1.17
2. Wind gusts	3σ	.15	.26	.13
3. Thrust misalignment	3σ	.25	.25	.25
4. Thrust and weights	3σ	.15	.15	.15
5. Pitch program	maximum	.50	.50	.50
^a Total		1.68	2.69	1.49

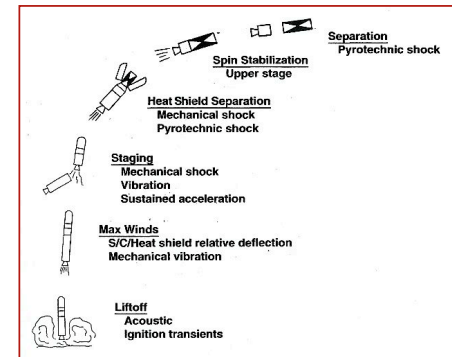
^aTotal consists of item 1 plus root sum square of items 2, 3, and 4.

Pitching Moment Distribution Causes Large Bending Effects



- Aerodynamic and thrust-vectoring effects bend the vehicle
- More on this in a later lecture

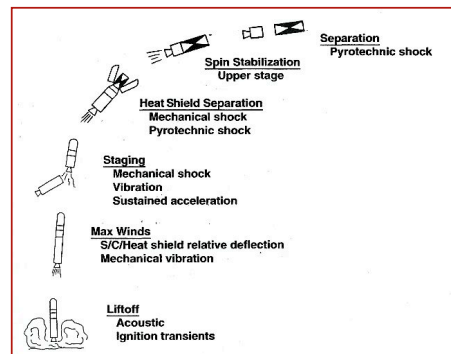
Launch Phases and Loading Issues-1



- **Liftoff**
 - Reverberation from the ground
 - Random vibrations
 - Thrust transients
- **Winds and Transonic Aerodynamics**
 - High-altitude jet stream
 - Buffeting
- **Staging**
 - High sustained acceleration
 - Thrust transients

Launch Phases and Loading Issues-2

- **Heat shield separation**
 - Mechanical and pyrotechnic transients
- **Spin stabilization**
 - Tangential and centripetal acceleration
 - Steady-state rotation
- **Separation**
 - Pyrotechnic transients



**Next Time:
Launch Vehicle Design:
Configurations and Structures**